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A Comprehensive Review on Distributed MPPT for Grid-Tied PV System: Sub-Module Level

Yousef Alharbi¹, Ahmed Darwish^{1*,} and Xiandong Ma¹

1	Lancaster	University,	School of	Engineering,	Lancaster,	United	Kingdom
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* Correspondence: a.badawy@lancaster.ac.uk

Abstract: The energy crises and the growth of the energy demand have increased the interest in 7 utilizing unconventional power sources. Thus, renewable energy sources have become a topic of 8 interest to mitigate the arising energy concerns and cope with the increased electricity demand. 9 With its remarkable merits including cleanness and abundance, photovoltaic (PV) solar energy sys-10 tems are a key player for solving these issues. The employed inverters should effectively utilize the 11 maximum available power from the PV solar system and transfer this power to the utility grid with-12 out posing any further limitations. However, the unequal power generation of the different PV sys-13 tems caused by Partial Shading (PS) and other PV panel degradation factors leads to reducing the 14 power system generation. One of the relatively new solutions to mitigate the mismatch concerns 15 between the PV modules and sub-modules is to extract the maximum power of each sub-module 16 individually. The main objective of this paper is to present a comprehensive review of such PV grid-17 connected inverters topologies associated with sub-module connections and control. It will classify 18 the PV grid-tied inverters in accordance with the level where the maximum power point tracking 19 (MPPT) system is implemented. A special focus has been placed on sub-module microinverters (MI) 20 in terms of circuit topologies, conversion efficiency, and controller design. This paper provides a 21 comprehensive analysis of employing the Distributed MPPT (DMPPT) approach to maximize the 22 power generation of PV systems and mitigate the mismatch issues between PV SM. The circuit to-23 pology, PV system configuration, and MPPT algorithms used for applying DMPPT solution at PV 24 SM are intensely discussed in this study. 25

Keywords: Photovoltaic (PV); Grid-connected Inverter; Power Electronic Converter; Grid-con-26nected systems; grid integration; MPPT technique.27

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1. Introduction

Nowadays, the electrical grid has evolved to become a mixture of several power-31 generating resources where photovoltaic (PV) generators are an important key player in 32 this integrated system [1,2]. Extracting the maximum power from the PV system and 33 studying the possible limitations of injecting the electrical energy into the grid is the key 34 design goal of grid-connected PV systems [3]. Thus, tracking the maximum power from 35 the PV systems during different irradiation levels, shading conditions, and low 36 conversion efficiency is one of the main design concerns [3,4]. Other several standards are 37 in place by different organizations to prevent overhead complications on the utility grid 38 [5-7]. For example, the power quality, reactive power control, and islanding operation are 39 of the main problems that pose severe issues for the distribution network. Therefore, the 40

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employed PV inverter should be designed so it is able to operate at a unity power factor,
improve the power quality, and have a fast dynamic response. Operating at a unity power
factor is important in order to reduce the total current through the cables and improve the
reactive power content in the grid [8].

From the power quality perspective, the major grid codes state that the total 45 harmonic distortion (THD) of the output current must not exceed the 5% limit [9]. The 46 THD is subject to increase by either the low or the high order current harmonics [10]. To 47 reduce the high order current harmonics, the employed inverter needs to operate at a high 48 switching frequency or to have big filtering elements in terms of inductors and capacitors. 49 Increasing the switching frequency puts more burden on the switching elements and may 50 increase the switching losses while making the filter bigger will increase the size and 51 volume of the system [11]. On the other hand, the low order harmonics can be eliminated 52 by the suitable control loops acting as harmonic compensators [12]. Figure 1 shows 53 experimental results for inverters producing outputs with high and low-order harmonic 54 currents. 55



Figure 1. Experimental results for inverters with; (a) high-order harmonic current and (b) low-order harmonic current (10 ms/div – 5A/div)

The fast dynamic response of the employed inverter will enable the system to recover 57 from faults swiftly, increasing the reliability against faults [13]. In addition, the design 58 must consider the islanding situation to protect both the users and equipment. The 59 conventional islanding method often monitors the grid parameters and takes prevention 60 actions accordingly [14]. Figure 2 shows another experimental test for an inverter 61 experiencing faults when its controllers have slow and fast dynamic responses. 62



(b)

(a)

Figure 2. Experimental results for inverters during faults with (a) slow dynamic response and (b) fast dynamic response (10 ms/div – 5A/div)

Categorizing the PV systems can be a helpful method for understanding the different 64 PV system architectures and the purpose of each design [14]. This might help researchers 65 in this field to comprehend the state of the art of grid-tied PV systems. The inverters and 66 MI are designed to convert the Direct Current (DC) to Alternating Current (AC) in both 67 large-scale PV plants and small PV applications, and it plays a crucial role in enhancing 68 the PV system reliability and improving overall efficiency [14]. Therefore, PV-interfaced 69 systems research is focused on optimizing the existing PV systems' topologies to reduce 70 PV system costs and achieve better system performance [15-20]. The PV system's design 71 usually comes in one of four common topologies according to the PV module 72 arrangements and PV system requirements. Namely, these topologies are centralized 73 inverter PV plants, string inverters, multi-string inverter PV, and PV module MI PV 74 systems [21]. 75

The conventional classification of PV systems is mainly based on the power capacity 76 of the PV applications and projects [21]. Thus, the three main categories of a grid-77 connected PV system are large-scale PV plants, medium-scale PV projects, and small-scale 78 PV applications. The small-scale application starts from a few kW to up to 50 kW, while 79 medium-scale project capacity can reach up to 1 MW. The PV system with a power 80 capacity of more than 1 MW can be considered a large-scale project [14,22]. 81

Classifying the grid-tied PV systems based on the voltage level at the point of 82 common coupling (PCC) is another approach to categorizing grid-connected PV systems. 83 Low Voltage grid-connected PV systems include both small PV applications and some 84 medium-scale PV projects where PV systems are installed close to the end users. Large PV 85 plants directly connected to a 20 kV voltage grid or more in high voltage grid-tied PV 86 systems [23]. One main objective of PV power converters devices is harvesting and 87 exporting the maximum available power from the PV system to the utility grid. Therefore, 88 designing and optimizing the maximum power point-tracking strategies can significantly 89 improve the PV system efficiency and enable obtaining the full available PV power [14, 90 25]. 91

The PV inverters are designed and controlled to operate on their maximum power 92 point (MPP) using the maximum power point tracking (MPPT) controller [26-32]. 93 Operating at the MPP of the PV system is usually related to the scale of the PV system. 94 This means that when the inverter or MI is connected to a few numbers of the PV modules, 95 the tracking process becomes swift and more accurate which can improve the efficiency 96 and reduce the overhead on the PV system controllers [25]. The grid-tied inverters are an 97 essential part of renewable energy interfaced systems that link the different types of 98 renewable resource and energy storage systems to the utility grid. Therefore, optimizing 99 the grid-connected inverters can significantly contribute to reducing the investment and 100 operation cost of the PV system [33]. 101

The electrical grids need support from the connected distributed generators and their 102 power generation security can be enhanced if the solar power plants can export the power 103 directly to the medium or high voltage networks without limiting grid stability [9,34]. 104 Controlling the active power of the PV system's current can increase energy yield and 105 enhance PV system performance, which can improve grid-side performance. However, 106 different power consumption patterns caused by changing the voltage and frequency of 107 the utility grid can negatively affect grid stability. Overcoming this issue will be based on 108 regulating the voltage and frequency during the design of the controllers of the grid-tied 109 PV systems [34]. The stability of the utility grid can be improved if proper active and 110 reactive power controllers are used, and common grid-related concerns especially voltage 111 sags can be solved [34-35]. 112

The grid-tied inverters can be interfaced with three-phase and single-phase power 113 systems according to the PV project size [35]. In the three-phase power system, the step-114 up transformers are used to boost the output voltage and meet the grid-side voltage 115 requirements [36-38]. Centralized inverters are usually used in three-phase power 116 systems to link large-scale PV plants to the utility grid [39]. The centralized inverter 117 technology is usually used in three-phase power systems and it might be the most 118 traditional in PV systems, also it has been used for many years because of its large-scale 119 conversion ability. On the other hand, in a single-phase power system, the small PV 120 applications are often interfaced with the distribution network, and Distributed MPPT 121 inverters are used [40]. 122

The Distributed MPPT inverters have been proposed to increase the power 123 harvesting from the PV systems. It can significantly increase power generation under low 124 irradiation levels. Also, distributing the MPPT can improve the scalability of the PV 125 system without introducing a significant disturbance to the utility grid. [33,40]. 126

The unbalanced power generation of PV modules due to the different environmental 127 conditions is one of the significant issues in centralized PV systems and it significantly 128 reduces power generation in PV systems [41, 43]. One main cause of unbalanced power 129 generation between PV components is partial shading due to buildings, clouds, and trees. 130 This can lead to mismatch problems in PV power systems. The mismatch problem can 131 negatively affect conversion efficiency since the PV system current will be limited by the 132 PV module with the lowest output current [42]. 133

Centralized grid-tide inverters might not be able to identify the power generated 134 by each parallel sting under a partial shading effect and the overall power generation of 135 the PV system will be reduced [43]. The bypass diode is commonly integrated with the 136 PV SM to minimize the effect of partial shading; however, it can cause multiple peak 137 power points. In such a scenario, the MPPT algorithm might be only able to track the 138 average maximum power. However, the average output power can be lower than the sum 139 of the maximum power of the PV modules [44]. 140

DMPPT technique has been used to mitigate the mismatch issue between PV 141 components and increase the energy yield of the PV system [45-47]. Although the DMPPT 142

strategy requires a more complex controlling process, it can improve the reliability of the 143 PV system and mitigate the mismatch problem [46]. 144

Several reasons can lead to the different current generations of PV components, 145 including external factors such as different PV panel orientations and partial shading. 146 Also, interior features like manufacturing tolerance and aging might lead to unbalance 147 power generation of PV strings [44]. Also, faulty PV components can limit the PV string's 148 current which will reduce the current generated by other PV components in the series 149 connection. Thus, processing the power generation of each PV component can mitigate 150 the negative effect of the faulty PV component on others in the series connection [45]. 151 Conventional PV systems have several severe problems that limit PV power generation 152 and adversely affect PV system performance. Power losses due to mismatch issues, partial 153 shading, and ground-associated faults can be the major issues. Thus, optimizing the 154 typical PV system is usually based on tackling these concerns. One proper solution to 155 overcome the mismatch concerns and partial shading effect is employing MPPT at a 156 finer level. This review paper discusses the state of the art of distributing MPPT 157 technology on grid-connected PV systems. It is focused on applying the DMPPT approach 158 at the PV SM level [48]. 159

One main objective of classifying the grid-connected inverter is to understand the latest 160 trend in this technology and help researchers to choose the optimization opportunities 161 effectively. Organizing the grid-tied inverters according to where MPPT is applied can be 162 a proper categorization strategy. In this review paper, the grid-connected inverters are 163 classified according to the level where the MPPT is applied. The grid-tied inverters can be 164 grouped into two main groups according to the MPPT function, Centralized MPPT, and 165 DMPPT. This work can be a helpful tool to understand different types of grid-connected 166 PV systems and the purpose of each PV system topology. 167

Some review papers have discussed employing the DMMPT approach to effectively 168 increase the power harvesting of PV systems [49]. Others discuss the negative effect of 169 partial shading on a group of PV cells [50]. However, none of them have deep discussions 170 about applying the DMPPT technique at the PV SM level. Thus, the lack of information 171 about employing DMPPT leads to this review paper. Although studies on [51] present 172 some issues related to DMPPT on the PV SM level, still there is an absence of discussion 173 about MPPT techniques used at the PV SM level. This paper reviews common power 174 converter topologies and MPPT techniques that have been used to employ the DMPPT 175 systems at the PV SM level. 176

This paper is reviewing the power electronic converter topologies used for grid-tied PV 177 systems, with a specific focus on low-voltage level modular PV applications. The paper 178 will categorize the grid-connected PV systems according to where MPPT is employed and 179 will explain the distributed MPPT strategy which has been used as a viable solution to 180 overcome the unbalanced power generation under the partial shading effect. A detailed 181 explanation of grid-tied PV inverter topologies including merits, limitations, and technical 182 issues is provided in section 2. An important consideration of PV SM DMPPT 183 architectures and a specific review of different MPPT algorithms is presented in section 3. 184

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2. Grid-Connected PV Inverter Topologies

study.

The grid-tied DC-AC inverters have been presented to enable pumping up the generated 190 power from PV systems into utility grid companies. To effectively send PV power to the 191 grid, several standards should be fulfilled by the grid-tied DC-AC inverter including 192 maintaining power quality, decoupling the arising AC current components at the input 193 side, and consideration of the islanding situation [52]. The DC-AC inverter is an essential 194 part of grid-connected PV systems and hence reducing the cost per inverter watt can 195 significantly minimize the installation cost of the PV generators. Therefore, many 196 researchers focus on innovating optimized and cost-effective inverters [53-55]. The 197 employed inverter can operate as a voltage or current source inverter [56]. For voltage 198 source inverters (VSIs), the input DC voltage will be chopped by input switches operating 199 and controlled by a pulse-width-modulation (PWM) scheme, converted to the output side 200 by the output switches and then filtered by inductors. 201

Detailed discussion about the finding of this review and proposed recommendations are

considered in section 4. Section 5 discusses the present associated challenges and gives

direction for related future work. Finally, section 6 concludes the outcomes of this review

The main issue with the VSIs is that their input currents are discontinuous which requires 202 large capacitors at the input side to smooth the PV module current [57]. Installing large 203 capacitors at the input side (output of the PV modules) is not favored as it can affect the 204 system's reliability negatively. The current source inverters (CSIs) can generate 205 continuous currents at the input side first, then chop the currents using the set of PWM 206 switches, and then filter this current using a capacitor [58]. The CSIs do not need large 207 filtering capacitors at the input side and therefore are favorable to be employed as PV 208 inverters. 209

However, their control system is usually more complicated than the VSIs and needs 210 careful parameter tuning. This is because the CSI requires at least an additional input stage 211 where the current is generated by the action of the input switches with the inductors. This 212 means that the output current and voltage are not generated directly from the input side 213 which appears as a right-hand plane (RHP) zero in the frequency domain analysis of the 214 inverter. Figure 3 shows the basic structures of VSI and CSI. 215



Figure 3. Generic configurations for dc/ac inverters: (a) VSI (b) CSI

The connection of the PV modules or panels to the inverters is important in selecting the217suitable inverter system. As shown in Figure 4, there are different possible connection218technologies and they will be presented briefly in the next subsections.219

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Figure 4. The grid-connected PV system classification according to DMPPT level (a) Single central PV inverter (b) Multi-central PV inverter (c) String PV inverter (d) PV module MI.

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2.1. Grid-Tied Central Inverter

The grid-connected central inverts might be the oldest technology used for both grid-tied 223 and standalone PV systems. The essential objective of the central inverters is to link the 224 high-power PV plants with the utility grid. The central inverter technology is a 225 combination of series and parallel connections of PV modules [59]. The series connection 226 is called a string and, it is used to generate sufficient output voltages according to the utility 227 grid needs. Thus, the central inverter does not necessarily require further voltage 228 amplification during the circuit design stage. Each PV string of the central inverter is 229 connected in parallel via string diodes to prevent the reverse current to flow from other 230 strings in the PV array. The parallel connection in central inverters is often used to obtain 231 the PV projects' high power requirements [60,61]. One common concern about the 232 centralized inverter is the self-partial shading of the PV system when some of the modules 233 cause shading to others. This issue can be solved by varying the distance from the PV 234 strings [62]. 235

The MPPT control of the grid-tide central inverter is usually operated at the PV plant level 236 which reduces the MPPT controllers' complexity. However, the central inverters have 237

several severe limitations, and one of the main concerns of this technology is the mismatch 238 losses due to the different power generation from the PV modules during the partial 239 shading conditions [63,64]. The central inverters often use high-voltage cables to link the 240 PV arrays with the utility grid, significantly increasing the installation cost. Also, the 241 scalability of the PV design is limited in this technology, thus increasing the power 242 production might not be achieved. The string diodes that are used in central inverters 243 have an internal loss that reduces the overall efficiency of the PV plants. The central 244 inverter malfunction might lead to the loss generated from the PV array [65]. 245

The breakdown of the central large-scale inverter can lead to stopping the entire PV system 246 from working, loss of PV power generation, and can pose several limitations to grid utility. 247 This concern can be mitigated by using multicentral PV inverters [68,69]. The multicentral 248 inverter topologies can improve the reliability of the large PV power plant and apply the 249 MPPT at a sub-array level which might mitigate the mismatch issues. The multicentral 250 PV inverter technology aims to group the large PV array system into subarrays where each 251 parallel connection is linked to an individual inverter. This technology is often preferred 252 for medium and large PV plants where power generation exceeds 0.5 MW [70]. The 253 multicentral PV inverters are commonly connected in parallel to obtain the maximum 254 power from the subarrays and maintain the reliability of the PV system in the case of 255 inverter malfunction. Figure 4 (a) illustrates the single central PV inverter topology and 256 Figure 4 (b) shows the multicentral PV inverter connection. 257

A basic example of central inverters is the three-phase VSI which is shown in Figure 5. 258 Because the full power is handled through the six semiconductor switches, the failure of 259 any switch will result in the full shutdown of the PV system. The switches can be affected 260 by overvoltage or overcurrent from the PV modules as well as the high temperature which 261 are expected in this application. This might increase power losses and adversely affect the 262 efficiency of the PV system. Distributing the MPPT at a lower level can mitigate this issue 263 and improve PV energy harvesting. 264



Figure 5. Three-phase VSI as an example of central inverters

The central inverter is usually a large inverter used to convert the high DC power from the267PV array to AC power. The system topology might come in one of two different topologies268in terms of power pressing, single-stage central inverter, and dual-stage central inverter.269Three-phase converters can offer some merits compared to single-phase full-bridge270

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converters including reducing the size of the high-frequency transformer with maintaining 271 the switching frequency, reduction in the size of filter components, and better conversion 272 efficiency [66]. The DC-AC central inverter is often connected to the medium and high 273 voltage power system because this technology is designed to generate high-rated power 274 which is more suitable to interface with a three-phase system. One of the main objectives 275 of using three-phase grid-tide central inverters is their capability to mitigate the effect of 276 THD and improve the transient performance, leading to higher efficiency [67]. On the other 277 hand, single-phase inverters will be required if the scale of the PV system is lower than 10 278 kW which is usually the limit of residential PV systems. The main issue with single-phase 279 systems is that they have pulsating power components at twice the grid's frequency. This 280 pulsating power will cause the input current of the inverter, which is the output current of 281 the PV modules, to have both dc and AC components. The AC current component will 282 cause the output PV power to be fluctuating around the MPP and hence the maximum 283 power will not be obtained, current-voltage and power-voltage curves are illustrated in 284 Figure 6. Therefore, the AC component of the inverter's input current has to be eliminated 285 using either a hardware filter or a complete control algorithm [12, 48]. 286



Figure 6. Generic current-voltage and power-voltage curves for a PV module

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2.2. Grid-Tied Distributed Inverter

The DMPPT is a strategy used to maximize PV energy harvesting and improve PV system 289 performance [45], [47]. The DMPPT approach can be implemented at different PV system 290 levels starting from the PV array level to the PV cell level [46]. The maximum energy of the 291 PV systems can be captured when the PV modules operate at their MPP as shown in Figure 292 6 while different tracking algorithms have been used to track and capture maximum power 293 from PV system [29-31]. The input voltage of the PV system should have relatively small 294 ripples to enable the tracking algorithm to operate successfully. To maintain the tracking 295 algorithm accuracy to become more than 98%, the voltage ripple from the PV input side 296 should be less than 8.5% [45]. 297

2.2.1. PV String Level Inverter

The string inverter technology in Figure 4(c) is an updated version of the conventional 299 central inverter topology [4]. Each string is built by connecting a series of PV modules and 300 the resultant connection is linked to the DC/AC inverter. Some string inverters can meet 301 the voltage requirements of the grid side and hence DC-DC step-up converter will not be 302 needed. However, some other systems will require DC-DC boost converters on the input 303 side or boosting transformers on the output side to step up the output voltage in order to 304 reach the voltage level of the utility grid [72]. Grid-tied string inverters can mitigate some 305 issues presented in central inverters [25]. For example, the power losses due to using the 306 string diode to eliminate reverse current from other strings of the parallel connection is 307 eliminated which helps to improve the overall efficiency of the PV system. Furthermore, 308 the mismatch issue between the PV system strings caused by different current generations 309 is reduced, and each PV string will operate at an individual MPPT [40]. Compared with 310 central inverters, the robustness of the PV system can be enhanced due to using string 311 inverters because failing one string does not lead to stopping the entire PV system from 312 working. Because the total power is shared by several inverters, the current ratings of the 313 employed semiconductor devices can be reduced in comparison with the central inverter 314 topology which will result in improving the efficiency and enhancing the reliability [49]. 315 Figure 4(c) illustrates the circuit topology of the string inverters. 316

2.2.2. PV Module Level Inverter

The conventional residential PV system topology is usually based on cascading the PV 318 panel to reach the grid-side voltage level. The maximum power can be harvested by 319 operating each PV panel at its total MPP which will be the global point for the combined 320 panel [73]. Nevertheless, residential PV applications are sensitive to the mismatch problem 321 between the PV panels because it adversely reduces PV power generation [4]. One 322 proposed solution to mitigate the mismatch problem between PV panels is to add a parallel 323 diode with each PV panel which can reduce the negative voltage polarity of faulty PV 324 modules caused by full or partial shading [74]. However, power generated from the 325 affected PV panel will be lost in this case. In the PV module level inverter system, each 326 separate PV module in the panel will have its dedicated inverter and controller to harvest 327 the maximum energy and operate the PV modules at their local MPPs. Accordingly, each 328 PV module will be sold with the MI which can be a single-stage or a double-stage inverter 329 [75]. Because the MIs are designed at the module level, the employed semiconductors can 330 have lower voltage and current ratings which will increase the total efficiency. Also, the 331 reliability of the total system will be improved during faults in one or more MIs because 332 the rest of the system will function normally. 333

Although it can be predicted that the cost of the system will be higher than the central 334 inverter structure, the study in [76] shows that the price can be lower on some occasions. 335 Moreover, this system provides more degree of freedom in terms of reactive power 336 generation and grid support in general. In this context, the DC-DC optimizer has been 337 proposed to obtain each PV module's power and meet the end users' local demands. The 338 DC-DC optimizer can be applied in two common topologies, series connected to DC-DC 339 optimizer and parallel connected DC-DC optimizer [77]. The cascaded DC-DC optimizer 340

architecture can provide better conversion efficiency compared with parallel connected341optimizers [78]. Figure 4(d) illustrates Module integrated DC-AC MI.342

2.2.3. PV Sub-Module Level DMPPT

This is a new approach to applying DMPPT in residential PV systems based on PV sub-344 panel level [23,72]. The integrated distributed power electronics enable capturing the 345 maximum power from each sub-panel inside a single PV module. Employing this strategy 346 not only reduces the current and voltage mismatch but also can increase the energy 347 capturing by up to 20 % by distributing MPPT at the finer level [72]. Commercial PV panels 348 are usually grouped into three or four groups according to the manufacturing company, 349 also the PV panel commonly comes with a PV junction box that contains the electronic 350 parts of the PV panel [23]. Figure 7 illustrates the typical 72 PV cell panel with its PV 351 junction box. 352



a) 72 Cells PV Panel

b) PV Panel junction box

Figure 7. A Standard 72 PV cells panel circuit diagram (a) The structure of the series connection of 72 solar cells PV panel (b) the Integrated junction box of the 72 cells PV panel.

The revolution of the grid-connected PV inverter is presented in Table 1. The past approach was based on conventional central inverter technology. The centralized inverter is commonly used with three phase power system. The MPPT system is implemented at the PV array level and only one MPPT is employed. The multi-string inverter technology comes after the central PV inverter. In such technology, the PV array is grouped into multi-strings. The MPPT is applied to a lower level and both three and single-phase power systems might be interfaced. In the PV string inverter DMPPT is implemented at the PV string level and a single-phase system is commonly used in this technology. The present technologies consist of a PV module and a PV SM inverter. Employing DMPPT at this level can significantly maximize power harvesting since the MPPT system is implemented at a finer level.

Ref.	DMPPT Level	Single/Three Phase	Voltage range (V)	Rated Power	PV interfaced Converter	Grid interfaced In- verter
[79]	Array	Three	380	20 Kw	Boost	Three Phase VIS
[80]	Multi-String	Three	180	1Kw	HFAC Link	Three Phase VIS
[81]	String	Single	110	1Kw	H-NPC	H- Bridge
[82]	Module	Single	230	1Kw	Cuk	H- Bridge
[83]	Sub-Module	Single	220	217W	Push-Pull	H- Bridge

Table 1. Com	parison of	various	grid-con	nected inv	erter topc	logies

3. PV SM DMPPT Architectures

3.1. Sub-Module MI

The harvested energy from the residential PV system can be significantly increased by 356 applying power conditioning to the sub-panel level [47]. Appling the DMPPT at the sub-357 panel level can mitigate the mismatch issue between sub-panels inside the same PV module, 358 increasing energy harvesting of the overall PV system [72]. Cascaded DC-DC optimizers 359 have been used to reduce the sub-panel mismatch problem and optimize the residential 360 PV system efficiency [72], [77]. However, the installation cost of this system might rise 361 when compared with the other types and also more complex controllers will be required. 362 Employing differential power processing (DPP) DC-DC converters is another strategy to 363 apply power conditioning at the PV sub-panel level [78], [84]. 364

The main objective of DPP converters is to equalize the photocurrent of the PV sub-panel 365 during the mismatch conditions. The complexity of the controlling process and the high 366 installation cost are the main drawbacks of this optimization method. Sub-module 367 microinverter (SMMI) can be a promising solution to effectively utilize the PV power from 368 each sub-panel and improve the total PV system's efficiency [85]. This futuristic strategy 369 can convert the DC current of the PV sub-panel to an AC current and link the output 370 current to the utility grid with no need for a central DC-AC inverter. Figure 8 illustrates 371 both series and parallel grid-connected MIs at the sub-panel level which will be presented 372 in the next subsections. 373

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a) Series Connected MI

b) Parallel Connected MI

Figure 8. Sub-Module grid-connected Micro inverter: (a) series and (b) parallel

3.2. Sub-Module Series Converters

The PV SM DC-DC optimizer proposed in [86] aims to increase energy capture of the PV 375 module during the unbalanced power generation of PV submodules. This study employed 376 a synchronous buck converter topology to mitigate the PV SM mismatch issue efficiently. 377 Low-cost devices with small sizes are used in the design stage due to increasing the 378 switching frequency range. The synchronous buck converters are cascaded to build higher 379 output voltage and avoid further step-up power converter circuits. The controlling process 380 of the SM DC-DC optimizer is relatively simple since no communication is required 381 between the SM controller during a mismatch effect. Figure 9 shows a schematic drawing 382 of the SM DC-DC optimizer. 383



Figure 9. Drawn diagram of the PV SM integrated MPPT system

In terms of MPPT control, each PV SM power is tracked using Preturbe and Observe (P&O) 385 algorithm. DC-DC optimizer strategy overcomes the several maximum points problem 386 caused by bypass diode under unbalanced power generation. The string current of the 387 three SMs can be considered a constant value since they are connected in series. Thus, the 388 controlling parameter used to track the maximum power point is the corresponding 389 voltage of each PV SM This becomes a direct optimization problem that aims to obtain the 390 maximum power by varying the duty cycle of each DC-DC optimizer. The flow chart in 391 Figure 10 illustrates the MPPT algorithm used to track the local MPP of each PV SM. 392

The local algorithm will start by initializing the parameters of the DC-DC converter. Then 393 it will sample the voltage output. Comparing the output voltage with the recorded 394 maximum voltage can determine the next step. If the duty-cycle ratio can achieve the 395 maximum output voltage, the first algorithm will stop and the output duty ratio will 396 become the input of the next tracking algorithm. Otherwise, the new duty ration will be 397 calculated by perturbing the first duty ration. After the approximate MPP is found by the 398 first algorithm, the P&O algorithm will be used to calculate the accurate MPP. The output 399 duty-cycle ratio from the first algorithm is used as the inial value of the second algorithm. 400 This duty ratio will be perturbed and voltage will be sampled accordingly. The direction 401 of the next tracking cycle can be decided by comparing the voltage of the current cycle 402 with the voltage of the previous tracking cycle. 403



Figure 10. The flowchart diagram shows the MPPT algorithms (a) the Global maximum point algorithm and (b) The typical P&O MPPT algorithm.

Zhu, et al. in [87] propose an SM single-inductor single-sensor DC-DC optimizer to reduce 405 the converter SM MI's size and cost. With only a single inductor and a single sensor, this 406 optimizer can make three SMs work on independent MPPs to maximize the energy 407 harvest. The suggested buck converters are connected in series to step up higher output 408 voltage. The MPPT algorithm used in this topology is the perturb and observe algorithm. 409 The major drawback of such a connection is that a single MPPT system is applied for the 410 three SMs of the PV panel. Thus, energy harvesting and PV system performance might be 411 negatively affected. Figure 11 shows the circuit configuration of the novel topology that 412 is based on a single inductor and single current sensor. 413



Figure 11. Configuration of the optimized buck-based MPPT system

To control the MPP of each SM, the adaptive perturb and observe (P&O) algorithm has 415 been used to perturb the PV module current and decide the direction of the next cycle. 416 The PV module current is sensed and compared to each SM's current which is used as the 417 reference current of the next tracking period. The duty-cycle ratio used for operating the 418 SM converters is calculated as the ratio between the SM current to the module current in 419 one tracking cycle. Figure 12 shows the flow chart of the adaptive MPP algorithm used in 420 this study where the clock parameter is a factor that decides which SM should be tracked. 421 The algorithm will start by sampling the PV SM current iL. 422

The clock value is regularly increased and decided which SM should be tracked. When 423 the value of the clock is between 0 and t the controller will track the MPP of the first SM 424 while the seconded SM MPP can be tracked if the clock value range from t and 2t. The 425 MPPT controller can track the third SM if the clock value is greater than 2t and less than 426 3t. The clock will reset after its value exceeds 3t. Once the controller decides which SM 427 should be tracked, the corresponding current of the tracked SM is divided by the PV 428 module current, and the result becomes the duty ratio of the SM DC-DC converter. 429



Figure 12. The flow chart illustrates the MPP algorithm according to the current of the PV SMs

3.3. Sub-Module Parallel Converters

The low voltage of solar cells makes the boost converter topologies more practical for 432 several PV applications. The boost converters are commonly used in parallel connection 433 to step-up the low voltage level to the grid voltage level. One of the common SM parallel 434 converters is a synchronous boost converter [88]. This topology aims to solve the SM 435 mismatch problem and effectively increase PV energy yield. The proposed converter is 436 based on connecting the SM-integrated converter in parallel. The MPP of each SM can be 437 captured individually to maximize energy harvesting and mitigate power loss. The 438 external connection between PV modules is in series to build up sufficient output voltage. 439 Figure 13 illustrates the circuit configuration of the SM parallel integrated converter. 440



Figure 13. The connection between the PV sub-module and sub-panel micro converters of a single PV panel

One MPPT microcontroller has been used to regulate the three SM on the PV panel since 442 the three converters are connected in parallel. Preserve and observe (P&O) tracking 443 algorithm used to track the MPP of each SM. The PV module output voltage is used as a 444 reference value to compare with SM voltages and then decide the direction of the next 445 tracking cycle. In every cycle of the tracking process, the three voltages of the SMs are 446 perturbed and compared with the output voltage. Figure 14 shows the MPPT controlling 447 algorithm flow chart used in [88]. 448

The first step of the MPPT algorithm is initializing the parameters of the tracking system. 449 Then the algorithm starts to measure the output voltage and PV SM voltage of three SM 450 voltages. The SM indices are deciding which SM voltage is controlled. The three SM 451 voltages will be perturbed continuously and the change of the output voltage of the PV 452 module will be recorded. The PV module will have three indices, but they are not shown 453 in Figure 14. The change in the output voltage of the PV module index will be measured 454 according to changes in SM voltages. The direction of the tracking cycle of each SM can 455 be decided according to the change of output voltage based on perturbing respective SM 456 voltage. The tracking algorithm will continue in the same direction, if a change in output 457 voltage is positive, else the direction of the tracking process will be reversed. 458



Figure 14. The flowchart shows the unified MPPT algorithm for capturing the MPP of PV submodules

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3.4. Sub-Module Differential Power Processing Converters.

In [89], Differential power processing DPP topology for PV SM MPPT implementation has 461 been proposed. This study employs DPP PV-PV topology with a bidirectional buck-boost 462 converter to solve the mismatch issue between the PV SM to maximize energy harvesting 463 and reduce power losses. The main objective of the proposed design is to efficiently 464 balance the current between the PV SM under unequal power generation. Figure 15 465 illustrates the DPP PV-PV architecture that is used to mitigate mismatch issues between 466 the PV SM. 467



Figure 15. The schematic diagram of the MI with DPP.

The P&O algorithm is employed to track the MPP. The DPP converter operates at a 469 relatively high frequency, thus the PV module voltage is assumed to be constant. Since 470the PV module voltage is assumed to be static, the PV module current is used as an 471 indicator to decide the direction of the next tracking cycle. The proposed topology in [89] 472 employs two loops to track the MPP. The fast-controlling loop operates the DPP buck-473 boost converters while the slower loop controls the DC-AC grid-tied inverter. Figure 16 474 shows the flow chart of the fast-controlling loop of DPP buck-boost converters. 475 The tracking algorithm will start by measuring the PV module current before perturbing 476 the duty-cycle ratio of the DC-DC converters. Then the DPP converter duty ratio will be 477

updated by adding a perturbing sample. The change of PV module current is sensed and
recorded after regularly varying the duty ratio of DPP converters. The new value of the
PV module current is compared with the previous value. When the PV module current
before perturbation is greater than the PV module current after perturbation, the direction
of the tracking process will change, otherwise, the tracking direction will not change.



Figure 16. The flowchart illustrates the algorithm for operating the DPP and balancing the current between PV SM.

Technical comparison results of some DMPPT topologies at the PV SM are illustrated in 483 Table 1. It summarizes power electronic devices that are used to obtain the maximum 484 power of PV SM. It illustrates that the P&O tracking algorithm is employed to track the 485 maximum power of PV SM for most proposed converters. This is to reduce the overhead 486 complexity of MPPT controllers. However, some research modified the conventional 487 P&O algorithm to enable tracking the maximum power of each SM using a single MPPT 488 system. It can be also noticed that several research has proven a significant increase in 489 power harvesting due to employing DMPPT at the PV SM level. From a power converter 490 perspective, it can be seen that several research relies on conventional power electronic 491 circuits including Buck, Boost, and flyback converters. Some others use DPP topologies 492 to equalize the current of the PV module by redirecting the SM current flow according 493 to the irradiation level. 494

Table 2. Comparison between different power electronic optimization studies to solve mismatch497issues inside an individual PV panel.498

Ref.	Rated Power (W)	Topology	Arrangement	MPPT Algorithm	Efficiency (%)	Improvements	Limitations
[86]	200 W	Synchronous Buck	Series	P&O	≈ 98	Increase power harvesting by (20 %)	Local Maximum point con- troller
[87]	-	Buck	Series	P&O	-	Less component	Single MPPT for three SMs
[88]	100 W	Synchronous Boost	Parallel	P&O	≈ 96	Improve efficiency due to using GaN technology	Operating regardless of mismatch condition
[89]	60W	Synchronous Buck-Boost	DPP	P&O	= 95	The capability of commer- cial inverter integration	Communication between neighboring DPP
[90]	60W	Bidirectional flyback	Parallel	-	≈ 98	Reduce mismatch level by (25 %)	A large number of current sensors
[91]	245W	DPP architec- ture with syn- chronous fly- back convert- ers	Parallel	DMPPT al- gorithm	_	Improve power extraction by 10.19%	Large storage element re- quired for decoupling pur- poses
[92]	-	DPP with central Boost	DPP	P&O	-	Accurate MPP tracking	Complex controlling pro- cess
[93]	-	Full Bridge Converter FBC	Series	P&O	-	Novel topology to apply DMPPT at a finer level	No experimental validation
[94]	300W	Synchronous Boost with Series Virtual Port DPP	DPP	Modified P&O	-	A single current sensor is required	More Components

5. Discussion and recommendation

Distributing the MPPT controller to obtain the maximum available power from each PV 500 SM individually enables maximizing the overall power generation of the PV module, 501 especially under the effect of the mismatch issue. The accuracy of the MPPT system is 502 improved due to employing The DMPPT approach at the PV SM level and the multiple 503 MPP problem caused by bypass diodes is significantly mitigated. The performance of PV 504 power electronic converters is slightly different according to the converters' 505 characteristics and the material used in the manufacturing process. The MPPT controller 506 techniques have been thoroughly reviewed in this study. This section presents a 507 discussion of the power converters for applying the DMPPT strategy to increase the 508 power generation of the PV module and improve the overall efficiency of the PV system. 509

The future associated power electronic converters used for employing the DMPPT 510 approach at the PV SM should expand to fulfill the technological development in the 511 power circuit topologies, the MPPT techniques, semiconductor materials, the power 512

quality requirements, and grid standards. The new power electronic devices should be513developed with fewer components, better efficiency, and reduced cost to effectively apply514the DMPPT approach at the PV SM level. These converters are expected to achieve the515following recommendations:516

The value of the input capacitors plays an important role in determining the lifetime of 517 the power electronic converters. Thus, introducing a new decoupling circuit is needed. 518 The new power electronic devices' efficiency should be improved due to applying soft 519 switching techniques. Soft switching technologies not only improve the PV system's 520 efficiency but it is also can increase the lifetime of the power electronic converters. 521

The power electronic switch is a basic element in the design of the power converters and 522 choosing switches with lower switching and conduction losses enables achieving better 523 efficiencies. It has been proven that GaN and SiC based power electronic switches can 524 achieve better efficiency and effectively minimize power losses. The on-state resistance 525 between the drain and the source of such switches is relatively low which minimizes the 526 conduction losses of the switch. Also, high switching frequencies are achievable with 527 minimal switching losses 528

In terms of power quality, galvanic isolation is not mandatory nowadays, however many 529 researchers consider it in the design stage since it protects against electrical faults. Anti-530 islanding detection is another feature that should be considered in the new designs, the 531 detection strategies should be swift and accurate to coop with the power grid failure. The 532 power quality is directly affected by THD, therefore the THD should be minimized to 533 improve the power electronic devices. The power quality discussion can not be completed 534 without emphasizing the importance of achieving and maintaining a unity power factor 535 system. 536

The development of a novel MPPT controller is important to maintain the voltage level 537 and help achieve the maximum available power from the PV side. The new MPPT 538 controllers should be able to pump up the extra power and maintain MPPT in the daytime 539 and enable compensation mood during night time. 540

5. Future Trend of the Grid-Tied MI

The partial and full shading effect on the PV systems can be unpredictable and 542 unavoidable in most scenarios. Partial shading might be a result of several conditions 543 including trees and building shadows, clouds, and birds dropping. The electrical 544 characteristics of the shaded part of the PV system become different from the unshaded 545 part. The percentage of irradiation level on the PV SM is directly proportional to the 546 amount of generated power. Thus PV SM with high irradiation level can generate more 547 power compared to PV SM with a low irradiation level. The PV system will be limited by 548 PV SM with the lowest irradiation level causing a mismatch between PV SMs. 549

The PV SM mismatches have a negative impact on the performance of the PV system. The series connection of the SMs results in limiting the PV module current by SM with the lowest output current. Harvesting each SM maximum power individually not only significantly increases power capturing of the PV module but also mitigates the power losses. DMPPT at the SM level aims to obtain the true available power by summing the individual maximum power of the three SMs of a single PV module. The new optimized 555

power electronic topologies are expected to be invented to further improve the PV system 556 performance and achieve better efficiencies. These topologies are needed to overcome the 557 currently associated limitations and provide reduced-size components. Large band-gap 558 devices such as GaN and SiC might be a promising solution to enhance the PV system 559 efficiency and use small components by allowing higher switching frequency. 560

One major issue that reduces the PV system power generation is the mismatch between 561 PV SMs during unbalanced power generation. The mismatch phenomena might occur as 562 a result of several reasons; however, partial shading can be the most common contributing 563 factor to this concern. The behavior of the PV SM is different according to the 564 environmental conditions of each SM. PV SMs are a part of the PV panel and they are 565 internally connected. Thus, applying the DMPPT strategy at the SM level requires 566 breaking the interconnection between SMs. Therefore, PV panel manufacturers might 567 revise the current PV panel electrical arrangement inside the PV panel junction box and 568 provide a new electrical layout considering the capability of integrating a new power 569 converter to implement DMPPT at the PV SM level. 570

Working at the PV SM level and adding optimized power electronic converters can 571 increase energy harvesting in different types of PV systems. The amount of harvested 572 energy extracted from the PV system can significantly increase when more DMPPT is 573 implemented among PV SM, especially under the partial shading effect. Proposing new 574 power electronic converters that offer better efficiency and improve the overall 575 performance of the PV system should be the focus of associated future work. Employing 576 these optimized power electronic converters at the PV SM can mitigate the mismatch 577 concerns and maximize power harvesting. 578

6. Conclusions

This paper discussed the DMPPT strategies which are used as a practical solution to 580 mitigate the mismatch problem in different types of PV system topologies. The DMPPT 581 approaches have been evaluated and compared for the PV string, PV module, and PV SM 582 systems. As the DMPPT is applied to a finer level, a more accurate MPP can be achieved, 583 and the mismatch loss issue can be effectively minimized. It has been concluded that the 584 most practical level where the DMPPT approach can be applied is the PV SM level. Thus, 585 the main focus of this paper is to evaluate and compare the different power electronics 586 converters used for applying DMPPT level at the SM level. Also, this study examines the 587 MPPT algorithm used to track the maximum power for different PV SM topologies. It has 588 been concluded also that most PV SM control designs use or modify the conventional P&O tracking algorithms to avoid further complexity in the PV system design stage.

This review paper presents a comprehensive comparison between different power 591 electronic converters that are used to implement the DMPPT approach at the PV SM. Alt-592 hough the P&O MPPT algorithm might be the most commonly used tracking algorithm 593 due to its simple implementation, the lack of tracking accuracy is a major concern of this 594 technique. The future research should focus on utilizing the new MPPT approaches such 595 as Artificial Intelligence (AI) and optimization algorithms approaches to improve the ac-596 curacy of MPPT methods. 597

Author Contributions

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